# Global sensitivity analysis for the boundary control of an open channel

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#### joint work with **Alexandre JANON**<sup>2</sup>, **Maelle NODET**<sup>3</sup>, and **Clémentine PRIEUR**<sup>3</sup> 1: CNRS, Gipsa-lab, Grenoble, 2: Univ. Paris-Sud, Math Labo

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Bienvenue à Grenoble pour les premières journées de l'Automatique

Let  $\mu = {\mu_1, \ldots, \mu_p}$  a random variable, modeling uncertainty parameters, a perturbed parameter, an unknown dynamics...

Let  $a(\xi, \mu) = 0$  be a Partial Differential Equation parametrized by  $\mu$  whose solution is  $\xi$ 

Let y be the to-be-controlled output: deterministic function:  $y = y(\xi)$ 

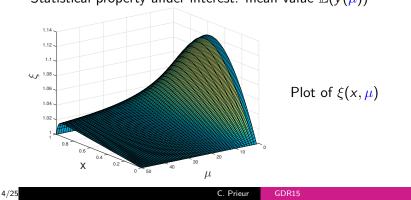
Natural question: What is the impact of random variable  $\mu$  on y?

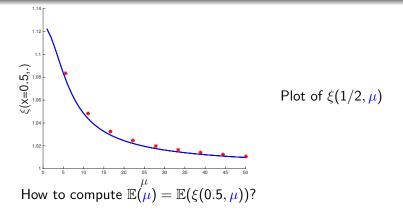
#### Toy-model

Consider

$$-\xi_{xx} + \mu \xi_x = 1$$
  
 $\xi(0) = \xi(1) = 1$ 

Assume  $\mu \sim \mathcal{U}(0, 50)$ , where  $\mathcal{U}(0, 50)$  is the uniform distribution on (0, 50). Define the *to-be-controlled output*:  $f(\mu) = \xi(0.5, \mu)$ . Statistical property under interest: mean value  $\mathbb{E}(\gamma(\mu))$ 





Bad idea Monte-Carlo estimator  $\mathbb{E}(\mu) \approx \frac{1}{N} \sum_{i=1}^{N} y(\mu^{i})$ with large N

Good idea If you compute a sample of e.g. 10 solutions, the 11th should be "close" to it  $\xi(., \mu^{11}) \approx \sum_{i=1}^{10} \lambda^i \xi(., \mu^i)$  and thus by computing the *to-be-controlled output*, we should find an estimation of  $\mathbb{E}(\mu)$ 

#### Goal: Global sensitivity analysis in a boundary control problem.

- the nonlinear **Shallow Water equations**: balance laws with effect of bottom slope and the slope's friction;
- the **boundary actions** are defined as the position of both spillways located at the extremities of the reach.

In [Coron, Bastin, d'Andréa-Novel; 08] & [Dos Santos, CP; 08], the authors designed stabilizing **boundary ouput feedback controllers**, with an **exponential convergence to the equilibrium** of water level and water flow.

**Issue**: we want to determine which factors (bottom slope, slope's friction, ...) are influent in this process. Je

The problem is related to probabilistic methods for control system design as considered by e.g., R. Tempo. Given  $\mu$  a vector of

random variables, define

 $f(\mu) = egin{array}{cc} +\infty & ext{if } G_\mu ext{ is unstable} \ \|G_\mu\|_\infty & ext{otherwise} \end{array}$ 

Consider the reliability estimation problem. Given  $\gamma > 0$ , estimate  $Pr\{f(\mu) \le \gamma\}$ 

Consider the **performance level estimation** problem. Given  $\varepsilon > 0$ , estimate  $\gamma$  such that  $Pr\{f(\mu) \leq \gamma\} \geq 1 - \varepsilon$ 

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## Outline

- 1 Modeling by means of Shallow Water equations when considering boundary actions, slope, friction...
- 2 Global sensitivity analysis (GSA) of uncertain physical parameters for boundary control stability of an open channel

3 Numerical results

#### First and total order Sobol indices

What are the most influent parameters on the output, when closing the loop? What about alone and combined impacts on the stability?

Use of a model reduction

4 Conclusion and perspectives

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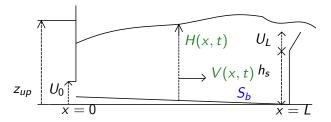
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One considers the classical Shallow Water equations for describing the flow dynamics inside an open-channel,  $\forall (x, t) \in [0, L] \times \mathbb{R}_+$ ,

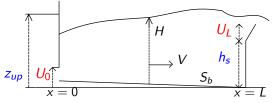
$$\partial_t \left( \begin{array}{c} H \\ V \end{array} 
ight) + \left( \begin{array}{c} V & H \\ g & V \end{array} 
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$$z_{up} \underbrace{I_{up}}_{X = 0} \underbrace{I_{up$$

The friction slope is given  $S_f = C \frac{V^2}{H}$ . Different models are possible (see in particular [Bastin, Coron, d'Andréa-Novel; 09] & [Dos Santos, CP; 08]). C is a constant friction coefficient



Denoting the channel width by *B* and the water flow by Q = BHV, the controls are the position  $U_0$  and  $U_L$  of both spillways:

• a submerged underflow gate:

$$Q(0,t) = U_0 B p_0 \sqrt{2g(z_{up} - H(0,t))}, \qquad (1)$$

• a submerged overflow gate:

$$H(L,t) = \left(\frac{Q^2(L,t)}{2gB^2\rho_L^2}\right)^{1/3} + h_s + U_L, \qquad (2)$$

where  $p_0$ ,  $p_L$  are water flow coefficients of the gates.

#### Linearization around an equilibrium

The steady state equilibrium of Shallow Water equations satisfies:  $V^{\star} = \left(\frac{S_b Q^{\star}}{BC}\right)^{1/3}, \quad H^{\star} = \frac{Q^{\star}}{BV^{\star}}.$ 

We first define

$$v(x,t) = V(x,t) - V^*$$
  
$$h(x,t) = H(x,t) - H^*$$

We then introduce the classical characteristic coordinates:

$$\xi_1(x,t) = v(x,t) + h(x,t)\sqrt{\frac{g}{H^*}} \\ \xi_2(x,t) = v(x,t) - h(x,t)\sqrt{\frac{g}{H^*}}$$

and the characteristic velocities:

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The linearized Shallow Water equations is

$$\partial_t \begin{pmatrix} \xi_1 \\ \xi_2 \end{pmatrix} + \begin{pmatrix} \lambda_1 & 0 \\ 0 & -\lambda_2 \end{pmatrix} \partial_x \begin{pmatrix} \xi_1 \\ \xi_2 \end{pmatrix} + \begin{pmatrix} \gamma & \delta \\ \gamma & \delta \end{pmatrix} \begin{pmatrix} \xi_1 \\ \xi_2 \end{pmatrix} = 0$$
(3)

with

$$\gamma = g C \frac{(V^{\star})^2}{H^{\star}} \left( \frac{1}{V^{\star}} - \frac{1}{2\sqrt{gH^{\star}}} \right) , \quad \delta = g C \frac{(V^{\star})^2}{H^{\star}} \left( \frac{1}{V^{\star}} + \frac{1}{2\sqrt{gH^{\star}}} \right)$$

Linear hyperbolic system of balance laws in Riemann coordinates. For suitable controllers, boundary conditions are simple. Indeed:

#### Proposition 1

Given any constant values  $k_0$  and  $k_L$ , defining the controls  $U_0$  and  $U_L$  by, for all  $t \ge 0$ ,

$$U_{0}(t) = \frac{H(0,t)\left(V^{*} - \frac{1+k_{0}}{1-k_{0}}(H(0,t) - H^{*})\sqrt{\frac{g}{H^{*}}}\right)}{p_{0}\sqrt{2g(z_{up} - H(0,t))}}$$
$$U_{L}(t) = -\left(\frac{H(L,t)\left(V^{*} + \frac{1+k_{L}}{1-k_{l}}(H(L,t) - H^{*})\sqrt{\frac{g}{H^{*}}}\right)}{\sqrt{2g}p_{L}}\right)^{\frac{2}{3}}$$
$$+H(L,t) - h_{s},$$

the boundary conditions (1) and (2) may be rewritten as

$$\begin{pmatrix} \xi_1(0,t) \\ \xi_2(L,t) \end{pmatrix} = \begin{pmatrix} 0 & k_0 \\ k_L & 0 \end{pmatrix} \begin{pmatrix} \xi_1(L,t) \\ \xi_2(0,t) \end{pmatrix} .$$
 (4)

Note that  $U_0$  and  $U_L$  depend only on water heights at both extremities of the channel.

Applying Lyapunov techniques, we may compute stabilizing controllers:

Proposition 2 ([Bastin, Coron, d'Andréa-Novel, 09])

For any  $(k_0, k_L) \in \mathbb{R}$  such that

$$\max\left\{|k_0|\sqrt{rac{\lambda_1\gamma}{\lambda_2\delta}},|k_L|\sqrt{rac{\lambda_2\delta}{\lambda_1\gamma}}
ight\}<1\;,$$

defining  $U_0$  and  $U_L$  with Proposition 1, the linear hyperbolic system of balance laws is exponentially stable, that is, it holds

$$egin{aligned} \|(\mathcal{H}(\cdot,t),\mathcal{V}(\cdot,t))-(\mathcal{H}^{\star},\mathcal{V}^{\star})\|_{L^{2}((0,L);\mathbb{R}^{2})}\ &\leq Me^{-
u t}\|(\mathcal{H}^{0},\mathcal{V}^{0})-(\mathcal{H}^{\star},\mathcal{V}^{\star})\|_{L^{2}((0,L);\mathbb{R}^{2})} \end{aligned}$$

where  $H^0$  and  $V^0$  stand for the initial conditions, and M,  $\nu$  are two positive values.

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$$\begin{split} \| (H(\cdot,t),V(\cdot,t)) - (H^{\star},V^{\star}) \|_{L^2((0,L);\mathbb{R}^2)} \\ & \leq \mathit{Me}^{-\nu t} \| (H^0,V^0) - (H^{\star},V^{\star}) \|_{L^2((0,L);\mathbb{R}^2)} \end{split}$$

where  $H^0$  and  $V^0$  stand for the initial conditions, and M,  $\nu$  are two positive values.

Remark In the previous result, we may consider other norms

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Global sensitivity analysis: How is the asymp. stability property impacted by the not well-known physical parameters?

## Let $\mu = (h_s, B, p_0, p_L, S_b, C, z_{up}, \xi_1^0, \xi_2^0)$ be the uncertain parameters,

i.e. random variables around the nominal values  $\mu_{nom} = \frac{1}{2} \left( \frac{1}{2} - \frac{1}{2} - \frac{1}{2} \right) \left( \frac{1}{2} - \frac{1}{2} - \frac{1}{2} \right)$ 

Name	Nominal value	$\mathcal{N}(m,\sigma)$ : normal distribution
		$\mathcal{U}(a, b)$ : uniform distribution
	4 <i>m</i>	$\mathcal{N}(4, 0.03)$
В	80 <i>m</i>	N(80, 1.03)
	0.65	$\mathcal{N}(0.65, 0.0066)$
$S_b$	0.0002	$\mathcal{N}\left(2 imes10^{-4}, 2.5 imes10^{-6} ight)$
С	0.001	$\mathcal{U}(9 \times 10^{-4}, 0.0011)$
Z <sub>up</sub>	10 <i>m</i>	$\mathcal{N}(10, 0.13)$
		initial state component $\mathcal{U}(-0.01, 0.01)$
$z_{up} \\ \xi_1^0 \\ \xi_2^0 \\ \xi_2^0$		initial state component $\mathcal{U}(-0.01, 0.01)$
$k_0, k_l$	0.6, 0.7	known
$Q^{\star},g$	50,9.81	known

GDR15

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hs	4 <i>m</i>	<i>N</i> (4, 0.03)
В	80 <i>m</i>	$\mathcal{N}(80, 1.03)$
$p_0, p_L$	0.65	$\mathcal{N}(0.65, 0.0066)$
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Given any constant values  $k_0$  and  $k_L$ , defining the controls  $U_0$  and  $U_L$  by Proposition 1 with  $\mu_{nom}$  instead of  $\mu$ , the boundary conditions (1) and (2) for with the parameters  $\mu$  are linearized as

$$\begin{pmatrix} 1 - \frac{\mathcal{B} + \sqrt{g/H^{\star}}}{2\sqrt{g/H^{\star}}} \end{pmatrix} \xi_1(0,t) + \frac{\mathcal{B} + \sqrt{g/H^{\star}}}{2\sqrt{g/H^{\star}}} \xi_2(0,t) = \mathcal{A}$$
$$- \frac{\mathcal{D} - \sqrt{g/H^{\star}}}{2\sqrt{g/H^{\star}}} \xi_1(L,t) + \left(1 + \frac{\mathcal{D} - \sqrt{g/H^{\star}}}{2\sqrt{g/H^{\star}}}\right) \xi_2(L,t) = \mathcal{C}$$

where  $\mathcal{A}$ ,  $\mathcal{B}$ ,  $\mathcal{C}$  and  $\mathcal{D}$  are values which depends linearly on  $\mu$ .

**Remark** Of course, if  $\mu = \mu_{nom}$ , then we recover the same boundary conditions than the previous ones for Riemann coordinates.

Definition of the *to-be-controlled output* (output of interest):

$$f(\mu) = \sqrt{\int_{t=0}^{T^*} \int_{x=0}^{L} \xi_1(x,t)^2 + \xi_2(x,t)^2 \,\mathrm{d}x \,\mathrm{d}t},$$

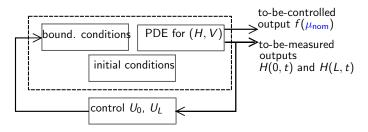
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Closed loop when they are no uncertainties

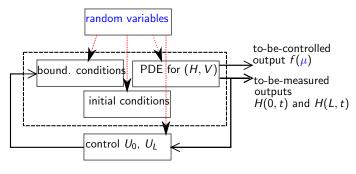
GDR15

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Closed loop in presence of random variables

## GSA by means of Sobol indices

The *to-be-controlled output* can then be considered as a scalar random variable  $Y = f(\mu)$ .

The conditional expectation  $\mathbb{E}(Y|\mu_i)$  is a random variable which gives the mean of Y over the distributions of the  $\mu_j$   $(j \neq i)$  Its variance quantifies the influence of  $\mu_i$  on the dispersion of Y.

The relative influence of  $\mu_i$  is given by the **first-order Sobol' index** 

$$S_{\{i\}} = rac{ ext{Var}\left(\mathbb{E}(f(\mu)|\mu_i)
ight)}{ ext{Var}(f(\mu))} \in [0,1]$$

Examples: If  $S_{\{i\}} = 1$ , then only  $\mu_i$  has an impact on YIf  $S_{\{i\}} = 0$ , then Y does not depend on  $\mu_i$ .

 $S_i^{total}$  measures the influence of  $\mu_i$  combined with other physical parameters in  $\mu$  on the output Y

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## How to compute $S_{\{i\}} = rac{Var(\mathbb{E}(f(\mu)|\mu_i))}{Var(f(\mu))}$ ?

For any  $i \in \{1, \ldots, p\}$ , let  $\mu_i^{j,1}$  and  $\mu_i^{j,2}$ ,  $j = 1, \ldots, n$  be two independent samples of size n of the parameter  $\mu_i$ .

We define:

$$\mu^{j,1} = (\mu_1^{j,1}, \dots, \mu_{i-1}^{j,1}, \mu_i^{j,1}, \mu_{i+1}^{j,1}, \dots, \mu_p^{j,1}) \quad j = 1, \dots, n$$
  
$$\mu_{\{i\}}^{j,2} = (\mu_1^{j,2}, \dots, \mu_{i-1}^{j,2}, \mu_i^{j,1}, \mu_{i+1}^{j,2}, \dots, \mu_p^{j,2}) \quad j = 1, \dots, n, \ i = 1, \dots, p$$

Let us consider the following quantities

$$Y^{j,1} = f(\mu^{j,1}) \quad j = 1, \dots, n$$

$$Y_{\{i\}}^{j,2} = f(\mu_{\{i\}}^{j,2}) \quad j = 1, \dots, n, \ i = 1, \dots, p.$$

To estimate all  $Y^{j,1}$  and  $Y^{j,2}_{\{i\}}$ , we have to evaluate (1 + p)n times the output, where n is the sample size.

#### Estimator of first order indices

Monte Carlo estimator: [Monod et al.; 06], [Janon et al., 14]

$$\hat{\mathbf{S}}_{\{i\},n} = \frac{\frac{1}{n} \sum_{j=1}^{n} \mathbf{Y}^{j,1} \mathbf{Y}^{j,2}_{\{i\}} - \left(\frac{1}{n} \sum_{j=1}^{n} \frac{\mathbf{Y}^{j,1} + \mathbf{Y}^{j,2}_{\{i\}}}{2}\right)^{2}}{\frac{1}{n} \sum_{j=1}^{n} \frac{(\mathbf{Y}^{j,1})^{2} + (\mathbf{Y}^{j,2}_{\{i\}})^{2}}{2} - \left(\frac{1}{n} \sum_{j=1}^{n} \frac{\mathbf{Y}^{j,1} + \mathbf{Y}^{j,2}_{\{i\}}}{2}\right)^{2}}.$$

Global Sensitivity Analysis, a many-query context: We have to evaluate (1 + p)n times the output  $\implies$  a model reduction is needed.

This reduction is done by using a metamodel, that is instead of considering the linear hyperbolic equation, we discretize it

#### Theorem

Assume that  $\mathbb{E}(Y^4) < \infty$ . Let  $\alpha \in (0,1)$  (typically  $\alpha = 0.05$  or 0.10). Then an asymptotic confidence interval of level  $1 - \alpha$  for  $S_{\{i\}}$  is given by

$$\left[\hat{\mathbf{S}}_{\{i\},n}-z_{1-\frac{\alpha}{2}}\frac{\hat{\sigma}_{\{i\}}}{\sqrt{n}},\hat{\mathbf{S}}_{\{i\},n}+z_{1-\frac{\alpha}{2}}\frac{\hat{\sigma}_{\{i\}}}{\sqrt{n}}\right],$$

with  $z_{1-\frac{\alpha}{2}}$  is the  $1-\frac{\alpha}{2}$  quantile of the  $\mathcal{N}(0,1)$  distribution and where  $\hat{\sigma}$  is any consistant estimator of  $\sigma_{\{i\}}$  defined by

$$\sigma_{\{i\}}^2 = \frac{\mathsf{Var}\left((Y - \mathbb{E}Y)(Y_{\{i\}} - \mathbb{E}Y) - \frac{\mathsf{S}_{\mathfrak{u}}}{2}\left((Y - \mathbb{E}Y)^2 + (Y_{\{i\}} - \mathbb{E}Y)^2\right)\right)}{(\mathsf{Var}Y)^2} \,.$$

Analogous result for  $S_i^{total}$ .

#### First-order Sobol' indices

 $T^{\star} = 75$ s, numerical results of the uncertain parameters  $\mu = (h_s, B, p_0, p_L, S_b, C, z_{up}, \xi_1^0, \xi_2^0)$ 

Parameter	95% confidence interval
hs	[0.090335; 0.11281]
В	[0.12559; 0.14833]
<b>p</b> 0	[-0.014771; 0.0078236]
<i>PL</i>	[0.27415; 0.29626]
S <sub>b</sub>	[0.067575; 0.090251]
С	[0.32127; 0.34233]
Z <sub>up</sub>	[-0.01477; 0.0078226]
$\xi_{1}^{0}$ $\xi_{2}^{0}$	[0.017666; 0.040285]
$\xi_2^{\bar{0}}$	[-0.0079254; 0.014667]

Thus, the parameters  $h_s$ , B,  $p_L$ ,  $S_b$ , C and  $\xi_1^0$  are influent on the *to-controlled-output* Y. C is the most influent one. The other parameter are not influent (with a confidence of 95%):  $p_0$ ,  $z_{up}$ ,  $\xi_2^0$ 

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#### What about the combined influence on Y?

Parameter	95% confidence interval for
hs	[0.098833; 0.11604]
В	[0.13818; 0.15573]
<b>p</b> 0	[-0.0077521; 0.0077808]
<i>p</i> L	[0.28348; 0.30269]
S <sub>b</sub>	[0.074616; 0.091309]
С	[0.33443; 0.35435]
Z <sub>up</sub>	[-0.007758; 0.0077727]
Ζ <sub>υρ</sub> ξ <sup>0</sup> ξ1	[0.025303; 0.041345]
$\xi_{2}^{0}$	[-0.0018308; 0.013773]

For each parameter, as the difference between the total and the first-order indices is not significant

## Total Sobol' indices

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It implies that the interactions are negligible. Thus the to-be-controlled output is additive in the parameters:

$$f_{discrete}(\mu) \approx \sum_{\mu_i \in \{h_s, B, p_0, p_L, S_b, C, z_{up}, \xi_1^0, \xi_2^0\}} g_i$$

where  $g_i$  are appropriate univariate functions. And even:



GDR15

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$$\begin{array}{lll} f_{discrete}(\mu) & \approx & \sum_{\mu_i \in \{h_s, B, p_L, S_b, C, \xi_1^0\}} g_i \\ & \approx & \sum_{\mu_i \in \{B, S_b, C\}} g_i \end{array}$$

## Conclusion, perspectives

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- Global sensitivity analysis (GSA) requires many evaluations of the output of interest, thus the need of model reduction
- GSA allows to determine which parameters are the most influent on a given *to-be-controlled output*
- B,  $S_b$ , C are the most influent parameters, with an additive effect.

#### Perspectives

- Analyze the sensitivity using the decay rate as the output?
- Considering the tuning parameters  $k_0$  and  $k_L$  as random variables, to find the "best" insensitizing controller?
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